Experimental and numerical study on fuel-NO_x formation in oxy-fuel processes in a jet stirred reactor

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1 Abstracts

New experimental results on fuel-NO_x formation in oxy-fuel processes are obtained in a jet stirred reactor. In the present work, effects of CO₂ (0~97.4%), temperature (873~1323 K) and equivalence ratio (0.56~1.61) on fuel-NO_x in oxy-fuel processes are experimentally and numerically researched. NH₃ is selected as the N element source. The predicted results by the PG2018 mechanism (Progress in Energy and Combustion Science, 67, 31-68, 2018) are consistent with the experimental results. Compared with N₂ diluted conditions, CO₂ increases in diluents can reduce NO formation in fuel-lean conditions and HCN formation in fuel-rich conditions. Under fuel-lean conditions, the NO formation path: NH₃→NH₂→HNO→NO weakens with the increase of CO₂ concentrations. Under the fuel-rich conditions, HCN is abundantly produced and reduced with the increase of CO₂. Moreover, the N₂O formation is basically insensitive to the CO₂ concentration.

Key words: oxy-fuel, fuel-NO_x, NH₃, Jet stirred reactor

2 Introduction

 CO_2 is formed from combustion processes and is the main source of greenhouse gas. The greenhouse effect has caused significant effects on global climate change. To meet this challenge and as an important step of carbon capture and storage, oxy-fuel combustion adopts O_2/CO_2 , not air, as a diluent. Thus, the CO_2 concentration in flue gas can be increased such that the efficiency of CO_2 capture is increased and the cost of CO_2 capture is decreased. Oxy-fuel combustion can reduce NO_x formation from N_2 because N_2 is separated. However, elemental N exists in solid fuel, such as coal and biomass. Elemental N in solid fuel is the main source for the combustion process. CH_4 and most elemental N are gasified in the devolatilization process. HCN and NH_3 in volatiles are the main source of fuel- NO_x . NH_3 is the primary fuel NO precursor in low rank coal volatiles¹. In the present study, a mixture of CH_4 and NH_3 simulates fuel containing elemental N.

To the best of our knowledge, numerous studies on fuel-NO_x in air atmosphere have been performed. Mendiara et al.² experimentally researched NO formation characteristics in a flow reactor at high CO₂ concentrations when NH₃ is selected as the N source. High CO₂ can reduce NO formation under fuel-lean conditions and promote NO formation under fuel-rich conditions. Tian et al.³ experimentally studied NH₃ transformation characteristics in a CH₄/NH₃/Ar/O₂ premixed flame in a McKenna burner. They found that NH₂ + O \leftrightarrow HNO + H, NH₂ + NO \leftrightarrow N₂ + H₂O and NH + NO \leftrightarrow N₂O + H exhibit important effects on NO formation. No studies have assessed NO and HCN formation characteristic in a 0D reactor when NH₃ is selected as an N source. JSR (jet stirred reactor) is a type of 0D reactor. When a reactant and oxidizer enter this reactor, intensive mixing is noted, approximately reaching a completely premixed and stirred state.

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Therefore, in the present study, the formation characteristics of fuel-NO_x in conventional and oxy-fuel conditions are studied in a JSR reactor. NH₃ is selected as the N element source. The effect of CO₂ concentration (0~97.4%), temperature (873~1323 K), and equivalence ratio (0.56~1.61) on fuel-NO_x formation in oxy-fuel processes are researched based on JSR experiments.

3 Experimental and numerical section

3.1 Jet stirred reactor



Figure 1. Schematic diagram of experimental facility: (a) system diagram, (b) picture of jet stirred reactor, (c) diagram of injects of jet stirred reactor

Figure 1 shows the experimental facility in the present work. Figure 1a is experimental system, including the gas supply system, electrically heated JSR reactor and measure system. As shown in Figure 1b, JSR consists of a 5-cm i.d. spherical fused silica sphere. Four injectors with nozzles of 1-mm i.d. are equipped for the admission of the gases to achieve stirring, as detailly shown in Figure 1c. The JSR is placed inside the electrically heated system at 1.5 kW surrounded by insulation material. In Figure 1b, Inlet 1 means the mixture of CH₄ and NH₃. The ratio of CH₄ to NH₃ is 5:1. Inlet 2 means the mixture of O₂, N₂ and CO₂. Gases in Inlet 1 and 2 are premixed and stirred in advance before entering the spherical reactor. The length of this regime from the Inlet of jet stirred reactor to the inside of the spherical reactor is 10 cm. The residence time in the regime is only 1/200 of that in spherical reactor, efficiently preventing reaction occurrence before entering the reactor. The thermocouple (Pt–Pt10%Rh, 0.25% T) is inserted in Inlet 4 to assess temperature inside reactor. The stability of the electrical heater and temperature uniformity inside reactor have been tested.

In the present work, gas purity is greater than 99.99%. The gas flow is precisely controlled by mass flowmeter. The gas component after reaction is tested on-line by FTIR (DX4000, Gasmet) with a resolution of 8 cm⁻¹ and scanning speed of 10 scans/s. Before entering the FTIR analyzer, the flue gas temperature is maintained at 180 °C. The concentrations of O₂, CO₂, NO, CO, HCN, N₂O can be tested by FTIR with \pm 1% error. In addition, O₂, CO₂, CO and NO concentrations are tested by an on-line gas analyzer (HORBIA PG350). Very good agreement between FTIR and PG350 analyses is noted for the compounds measured by both technologies (CO, NO and O₂).

2.2 Conditions setting

All conditions in the present work maintain total flow at 1 dm³/min (STP). CH₄ is 5000 ppm, and NH₃ is 1000 ppm. For the present work, both CH₄ and NH₃ can react with O_2 , i.e.,

 $x \text{ CH}_4 + y \text{ NH}_3 + (2x + 1.25y) \text{ O}_2 \rightarrow x \text{ CO}_2 + y \text{ NO} + (2x + 1.5y) \text{ H}_2\text{O}$

Therefore, the equivalence ratio is defined as

$$\Phi = \frac{(CH_4 + NH_3)/O_2}{[(CH_4 + NH_3)/O_2]_{stoic}}$$

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Cases $1\sim2$ are used to study the effect of temperature under an oxy-fuel atmosphere. The temperature is 873~1323 K. Cases $3\sim5$ are used to study the effect of the equivalence ratio under oxy-fuel atmosphere with an equivalence ratio of 0.56~1.61. CO₂ concentrations in diluent are 0, 0.3 and 0.6, respectively at Case 3, 4, 5. The detailed settings are listed in Table 1.

Table 1 Experimental conditions setting				
Case	O ₂ -%	CO ₂ -%	T-K	Φ
1	2.0,1.13,0.7	0	873~1323	0.56,1.0,1.61
2	2.0,1.13,0.7	30	873~1323	0.56,1.0,161
3	2.0~0.7	0	1273	0.56~1.61
4	2.0~0.7	30	1273	0.56~1.61
5	2.0~0.7	60	1273	0.56~1.61

2.3 Numerical model

Numerical results are calculated through the PSR module in CHEMKIN PRO. AURORA code is adopted to perform chemical kinetics analysis. The reaction conditions in simulation process are consistent with that in experiments. The chemical mechanism (151 species, 1397 reactions) used in the work is put forward in the review about N components by Glarborg et al.⁴. This mechanism combines studies published over the last 40 years regarding N-containing chemical mechanisms based on the work of Miller et al.⁵. Predicted results based on this new mechanism are consistent with the experimental results with the exception of NO in high CO_2 atmospheres in fuel-rich cases.

3 Results and discussions

3.1 Effect of CO₂ concentration



Figure 2. Profiles of NO, HCN, N₂O in oxidation process of CH₄ and NH₃ under 1273 K at different CO₂ (0~100%) and different equivalence ratio (a) 0.6; (b) 1.0; (c) 1.6

Figure 2 shows the profiles of NO, HCN and N₂O in different CO₂ concentrations in dilutions and different equivalence ratios at 1273 K. Under fuel-lean conditions (Φ =0.6), when CO₂ is 0 in diluent, the NO formation is 160 ppm. In fuel-lean conditions, as the CO₂ concentration increases, NO formation gradually decreases. In this case, HCN formation is approximately zero. The formation of N₂O gradually increases as CO₂ increases but is still maintained at approximately 15 ppm. Under stoichiometric conditions (Φ =1), NO formation decreases at all CO₂ concentrations compared with that in Φ =0.6. The formation of N₂O decreases to less than 10 ppm. HCN formation is greater than 5 ppm. Under fuel-rich conditions (Φ =1.6), N₂O formation is approximately zero. For NO formation in this case, NO formation reaches 50 ppm. However, the mechanism adopted in the work poorly predicts NO formation in fuel-rich conditions. Under Φ =1.6, when the diluent is N₂, HCN formation is greater than 260 ppm. When the CO₂ concentration in diluent is 30%, HCN formation is sharply decreased to 46 ppm. As CO₂ increases further, less HCN is formed. Through simulation, when the CO₂ concentration in the diluent increases to 100%, HCN formation plateaus at zero.

Based on rate-of-production analysis under Φ =0.6 and 1273 K, the conversion rate of NH₃ to NO or N₂ through different path are analyzed and shown in Figure 3. $NH_3 \rightarrow NH_2 \rightarrow HNO \rightarrow NO$ is the first important path of NO formation under Φ =0.6 and 1273 K. When the diluent is N₂, the conversion rate of this path is greater than 25%. As the CO₂ concentration in diluent increases from 0 to 100%, the conversion rate of this path decreased to 17%, mainly because the increased CO₂ concentration weakens NH₂+O \leftrightarrow HNO+H, according to the sensitivity analysis. Among the six NO formation paths, $NH_3 \rightarrow NH_2 \rightarrow H_2NO \rightarrow HNO \rightarrow NO$ strengthens as CO_2 increases mainly because the increased CO_2 concentration enhances $NH_2+HO_2 \leftrightarrow$ H_2NO+OH . However, this path is not the main path for conversion of NH_3 to NO. When CO_2 in the diluent increases to 100%, the conversion rate of this path increases to only 6%. For NO formation, increased CO₂ inhibits NO formation. As shown in Figure 4, $NH_3 \rightarrow NH_2 \rightarrow N_2$, is the first important path of NH_3 transformation to N_2 . As the CO₂ concentration increases from 0 to 100%, the conversion rate of this path increases from 18% to 22%, mainly because the increased CO₂ concentration enhances NH₂+NO \leftrightarrow N_2 +H₂O, according to the sensitivity analysis. As the second important pathway for transformation of NH₃ to N₂, NH₃ \rightarrow NH₂ \rightarrow NNH \rightarrow N₂ also increases from 10% to 13% as the CO₂ concentration increases from 0 to 100%. Because the increased CO₂ concentration enhances NH₂+NO \leftrightarrow NNH+OH and NNH \leftrightarrow N₂+H. Comprehensively, under fuel lean conditions, NO decreases as CO_2 increases in the diluent for two main reasons: (1) the transformation of NH_3 to NO is weakened; (2) the transformation of NH_3 to N_2 is strengthened.





3.2 Effect of equivalence ratio



Figure 4. Experimental (symbols) and simulation (lines) results of NO, HCN and N₂O as a function of equivalence ratio (0.56~ 1.61) diluted by different CO₂ in diluent (0,30%). The inlet conditions correspond to case 3 and 4

Figure 4 presents profiles of NO, HCN and N₂O concentrations as a function of equivalence ratio (0.56~1.61) under 1273 K and different CO₂ concentrations in diluent (0 and 30%). Generally, under N₂ and 30% CO₂+70% N₂ atmosphere as the equivalence ratio increases, NO and N₂O concentrations gradually decrease. The HCN concentration initially increases and then decreases. Under N₂ atmosphere, the HCN peak occurs at Φ =1.45. However, under 30% CO₂+70% N₂, the HCN peak occurs at Φ =1.4. When $\Phi \ge 1$ and <1.4, significant NH₂ is formed and promotes HCN formation. When $\Phi \ge 1.4$, NH₂ is transformed to NH₃. Less NH₂ is transformed to HCN.

3.3 Effect of temperature



Figure 5. Experimental (symbols) and simulation (lines) results of NO,HCN,N₂O as a function of temperature (800~1400 K) at different equivalence ratio (0.56,1.0,1.61) and different CO₂ concentration in diluent (0,30%). The inlet conditions correspond to case 1 and 2

Figure 5 presents the profiles of NO, HCN and N₂O as a function of temperature (800~1400 K) under different equivalence ratios (0.56 (a1,b1,c1), 1.0 (a2,b2,c2), 1.61 (a2,b2,c2)) and different CO₂ concentrations in diluent (0 (red), 30% (blue)) in a JSR reactor. For NO formation under fuel-lean conditions whether in conventional processer or oxy-fuel processes, NO formation gradually increases as the temperature increases. Under Φ =0.56, NO formation begins at 1000 K. When 30% CO₂ is added to diluent, NO formation decreases by approximately 50 ppm. Under Φ =1, NO formation begins at 1100 K. The addition of 30% CO₂ decreases NO formation to less than 10 ppm. In Φ =0.56 and 1, increased temperature increases NO formation. According to sensitivity analysis and production rate analysis, NH₂+NO \leftrightarrow N₂+H₂O is weakened and HNO(+M) \leftrightarrow H+NO(+M) is strengthened under oxy-fuel processes as temperature increases.

Under fuel-rich conditions, compared with Φ =0.5 and 1, less NO is formed. Under conventional conditions, as temperature increases, NO formation increases at first and later decreases, reaching the peak at 1150 K. However, under oxy-fuel processes (30% CO₂+70% N₂), more NO is formed as the temperature increases. The simulated results under fuel-rich conditions are not consistent with experimental results.

Regarding N₂O formation in reaction processes, as the temperature increases, N₂O formation increases at first and then decreases. At Φ =0.56, the N₂O peak occurs at 1100 K and is approximately 30 ppm. At Φ =1, the N₂O peak occurs at 1250 K and is approximately 15 ppm. At Φ =1.61, minimal N₂O is formed. Compared with N₂ atmosphere, N₂O formation exhibits no obvious difference in oxy-fuel processes. According to sensitivity analyses and rate-of-production analyses, NH+NO \leftrightarrow N₂O+H and N₂O(+M) \leftrightarrow N₂+O(+M)

control N₂O formation. At temperatures greater than the critical temperature, N₂O(+M) \leftrightarrow N₂+O(+M) sharply increases. At higher temperatures, N₂O is decomposed.

For HCN formation, under fuel-lean conditions (Φ =0.56), HCN occurs at a regime of 1000~1200 K because CH_x forms from underoxidized CH₄. CH_x reacts with NH₂ to form HCN through NH₂ \rightarrow CH_xNH_y \rightarrow (H₂CN,HCNH) \rightarrow HCN. Under fuel-rich conditions (Φ =1.61), HCN formation begins at 1150 K. Under N₂ atmosphere and as the temperature increases, HCN increases at first and then decreases, reaching the peak at 1250 K. However, under oxy-fuel conditions (30% CO₂+70% N₂), more HCN is formed as the temperature increases. In general, HCN in oxy-fuel conditions (30% CO₂+70% N₂) is reduced compared with conventional conditions. Under fuel-rich conditions, CH₄ oxidation is insufficient, and CH_x is formed.

4 Conclusions

In the present work, the effect of CO_2 concentration (0~97.4%), temperature (873~1323 K), and equivalence ratio (0.56~1.61) on NO, N₂O and HCN formation in oxy-fuel processes are experimentally researched in a JSR reactor. NH₃ is selected as the source of N element. The results predicted by PG2018 are consistent with the experimental results. Based on experimental and numerical results, the following conclusions can be made:

(1) The main fuel-NO formation path is $NH_3 \rightarrow NH_2 \rightarrow HNO \rightarrow NO$, regardless of N_2 or CO_2 as diluent. The NO-reburning chemistry cannot be ignored and it can even reduce the majority of NO at fuel-rich conditions. With the increase of CO_2 concentration, the fuel-NO foramtion path strengthens and the NO-reburning chemistry weakens, lending to the decrease of NO;

(2) For the formation of NO, under fuel-lean conditions, it increases with the increase of temperature from 1100 K to 1400 K. Under the stoichiometric condition, the NO productions from N_2 and CO_2 atmospheres are nearly the same. Under fuel-rich conditions and temperatures above 1200 K, the high CO_2 concentration enhances the NO production due to the reduced NO-reburning chemistry;

(3) For the formation of HCN, it is formed mainly through the pathway of $NH_3 \rightarrow NH_2 \rightarrow CH_xNH_y \rightarrow (H_2CN, HCNH) \rightarrow HCN$ and the CH_x radical is significant for the HCN production;

(4) Although the reaction is slightly delayed under high CO₂ concentration, the N₂O formation is basically insensitive to the CO₂ concentration, because the main N₂O formation reactions of NH+NO \leftrightarrow N₂O+H, N₂+O(+M) \leftrightarrow N₂O(+M) and N₂O(+M) \leftrightarrow N₂+O(+M) are insensitive to the variation of the CO₂ concentration, regardless of temperature, equivalence ratio;

(5) For the present study, the prediction by PG2018 is found to be consistent well with the overwhelming majority of the present experimental data under both N₂ and CO₂ atmospheres. Important reactions such as NH₂+O \leftrightarrow HNO+H, HNO+OH \leftrightarrow NO+H₂O and NH₂+NO \leftrightarrow N₂+H₂O are identified for future development of the fuel-NO_x mechanism, especially for fuel-rich conditions under high CO₂ concentrations.

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