# Effects of Hydrogen Peroxide on Methane Premixed Flames

Guan-Bang Chen<sup>1,\*</sup>, Yueh-Heng Li<sup>2</sup>, Tsarng-Sheng Cheng<sup>3</sup>, Hung-Wei Hsu<sup>3</sup>, Yei-Chin Chao<sup>2</sup>

<sup>1</sup>Research Center of Energy Technology and Strategy, National Cheng Kung University Tainan, 701, Taiwan, ROC
<sup>2</sup>Department of Aeronautics and Astronautics, National Cheng Kung University Tainan, 701, Taiwan, ROC
<sup>3</sup>Department of Mechanical Engineering, Chung Hua University Hsinchu, 300, Taiwan, ROC

# **1** Introduction

Lean combustion is generally considered as a timely solution for the more stringent environmental regulations and global weather concerns in the new century. However, lean combustion is suffered to combustion instability, such as flame pulsation, flame blowout and flickering, due to low heat release rate and high local extinction. It turns out to release high CO and UHC (unburned hydrocarbon) emissions in lean combustion application. Some strategies for stabilizing lean premixed flames and extending lean flammability limit have been proposed in decades [1-3]. Altering chemical characteristics in flames is one of successful manners to sustain lean combustion. For example, utilizing catalyst in combustors [4] and adding strong oxidant to fuels [5] are common approaches. Employing active fuel or adding strong oxidant to fuels is subject to increase flame temperature and reactive radicals in flames, and then to further stabilize lean combustion. Nevertheless, hydrogen peroxide ( $H_2O_2$ ) is an environmentally friendly oxidant with strong oxidability. Even after chemical dissociation, hydrogen peroxide produces only oxygen and steam.

A few recent studies have indicated some potential promises in utilizing hydrogen peroxide for improving practical combustion process. Golovitchev et al. [6] examined the possibility of promoting methane auto-ignition in air using 5-10% hydrogen peroxide. Ting and Reader [7] used PREMIX code to investigate the effects of hydrogen peroxide on the premixed methane-air flame under atmospheric conditions. Hydrogen peroxide was found to be effective in enhancing the burning velocity, and this was particularly true for the richer mixtures considered. Kim et al. [8] discovered that hydrogen peroxide assisted the conversion of harmful nitric oxide to nitrogen dioxide in diesel exhaust gas. In addition, Born and Peters [9] found that proper injection of hydrogen peroxide into a diesel engine reduced soot and NOx drastically. Martinez et al. [10] reported that the concentrations of UHC, CO and NOx from their industrial pilot plant scale combustion chamber fueled with natural gas were lowered significantly by the injection of a few hundred ppm of hydrogen peroxide. Based on the above studies, promotion to stable lean combustion is more effective with the addition of hydrogen peroxide

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than that with hydrogen addition. Hydrogen is considered as an easy-ignited fuel and helpful for increasing flame temperature. But, hydrogen peroxide is as a reactive stimulator or an oxidizer to shift chemical pathways and to further enhance chemical radicals.

This study numerically examines the effects of hydrogen peroxide on premixed methane-air flames using CHEMIKIN Collection with GRI-Mech 3.0 chemical reaction mechanisms [11]. Numerical results indicate the addition of hydrogen peroxide affects the reaction pathway, laminar burning velocity, flame temperature, and pollutant formation.

#### 2 Numerical Method

In this work, the PREMIX code of Chemkin collection 3.7 is used to calculate the adiabatic, unstrained, free propagation velocities of the laminar premixed  $CH_4/air/H_2O_2$  flames. It solves the steady-state comprehensive mass, species and energy conservation equations for the planar flame. In addition, the adiabatic flame temperature is calculated by using the EQUIL code. The GRI-Mech 3.0 chemical kinetic mechanisms and detailed transport properties are used without any modifications. The unburned reactants are supplied at 423 K and 1 atm. This temperature is the boiling temperature of  $H_2O_2$  and it will make reactant to be in gas phase.

Simulations were performed for three different conditions: (1) replacing partial air by  $H_2O_2$  (2) adding  $H_2O_2$  as fuel additive (3) using  $H_2O_2$  as an oxidizer but with different concentrations. The decomposition of one mole  $H_2O_2$  will produce 0.5 mole  $O_2$  and one mole  $H_2O$ . Therefore, the stochiometric  $CH_4/H_2O_2$  ratio is 0.25 and the global reaction is defined as:

$$CH_4 + 4H_2O_2 \rightarrow CO_2 + 6H_2O \tag{1}$$

In the case of replacing partial air by  $H_2O_2$ , the total  $O_2$  is maintained to keep the equivalence ratio constant but  $N_2$  will be decreased. In the case of adding  $H_2O_2$  as fuel additive, the maximum ratio of  $H_2O_2$  to methane is 100%. In the last case of using  $H_2O_2$  as an oxidizer, the concentration of  $H_2O_2$  is varied from 30 to 100%.

## **3** Results and Discussion

The temperature and species concentration profiles of the premixed stoichiometric CH<sub>4</sub>/air and CH<sub>4</sub>/85% air /15% H<sub>2</sub>O<sub>2</sub> are shown in Fig.1. Results indicate that the permixe flame with 15% air replaced by hydrogen peroxide has a higher adiabatic flame temperature due to heat-released from thermal decomposition of hydrogen peroxide. In addition, the increase of  $H_2O_2$  content in air results in an increase of water production, but decreases the carbon dioxide formation. On the other hand, some intermediate radicals, such as CO, OH, H, O, and HO<sub>2</sub> etc, show the increasing trends. These facts suggest that the dominate reaction path of methane combustion is altered by  $H_2O_2$  effect. Figure 2 shows the effect of replacing partial air by H<sub>2</sub>O<sub>2</sub> on laminar burning velocity and adiabatic flame temperature for three different equivalence ratios (ER). It can be seen that the laminar burning velocity increases with increasing the replacement of air with H<sub>2</sub>O<sub>2</sub>. As air is completely repalced wih  $H_2O_2$ , the laminar burning velocity approaches to 4.7 m/s for ER = 0.6, 0.8, and 1.0. This is due to that the oxidizer is completely provided from hydrogen peroxide decomposition and hydrogen peroxide dominates the reaction rate of methane. The adiabatic flame temperature is also increased with increasing the replacement of air with H<sub>2</sub>O<sub>2</sub>. The maximum increased temperature is about 900 K for ER = 0.6 flame, which is higher than the increased temperature for ER = 0.8 and 1.0 flames. The increased temperature is due to that the heat released from hydrogen peroxide decomposition is much higher than that released from methane reactions.

Figure 3 indicates the effect of  $H_2O_2$  concentrations on laminar burning velocity and adiabatic flame temperature of stiochoimetric  $CH_4/H_2O_2$  flames. Results show that with 30 vol.% of  $H_2O_2$  the laminar burning velocity is slightly higher than that of the stoichiometric  $CH_4/air$  flame, but the adiabatic flame temperature is lower by about 250 K. When the  $H_2O_2$  concentration is increased to 40 vol.%, the adiabatic flame temperatue is about the same as that of the stoichiometric  $CH_4/air$  flame. Nevertheless, the laminar burning velocity is increased to 1.57 m/s, which is twice higher than that in stoichiometric

condition (0.72 m/s). It means that the existence of hydrogen peroxide in premixed methane flame not only generates thermal effect, but also results in chemical effect. Figure 4 shows the effects of  $H_2O_2$ additions to methane fuel on the laminar burning velocity and adiabatic flame temperature of the  $CH_4/H_2O_2/air$  flames with ER = 0.6, 0.8, and 1.0. It can be seen that the laminar burning velocity increases with increasing the  $H_2O_2$  concentrations, especially for the case of ER = 1.0. However, the adiabatic flame temperature remains relatively constant for three different equivalence ratios studied. It is noted that the increase of  $H_2O_2$  concentrations from 0 to 100% increases the laminar burning velocity by 42% for ER = 1.0 flame. When ER = 0.6, the laminar burning velocity is increased only by 26%. Comparisons of Figs. 4 and 2 suggest that the addition of small amount of  $H_2O_2$ to fuel has lesser effect on the laminar burning velocity and adiabatic flame temperature than the replacement of air with  $H_2O_2$ . The effects of  $H_2O_2$  on the OH, CO, NO and NO<sub>2</sub> formations in three different hydrogen peroxide adding approaches are investigated as shown in Figs. 5-8. The increase of OH concentration in flames manifests the severe chemical reactions, especially for the case of H<sub>2</sub>O<sub>2</sub> as an oxidizer. OH concentration increases significantly when the  $H_2O_2$  as an oxidizer is increased to 60% (see Fig. 5c). It elucidates that the hydrogen peroxide effect consists of thermal and chemical effects. The addition of extra  $H_2O_2$ to fuel results in insignificant effect on OH formation (Fig. 5b).

Figure 6 shows that the CO concentration increases drastically in the preheat zone and then decreases in the reaction zone. The replacement of partial air with  $H_2O_2$  increases CO formation (Fig. 6a). Whereas additing extra  $H_2O_2$  to fuel decreases CO formation (Fig. 6b). CO concentration increases significantly when the  $H_2O_2$  as an oxidizer is increased to 60% (Fig. 6c). As to NO<sub>x</sub> emission, Figs. 7 and 8 show that both NO and NO<sub>2</sub> concentrations increase with either replacing partial air by  $H_2O_2$  or adding extra  $H_2O_2$  to fuel. The enhancement of NO<sub>x</sub> production is due to the increased flame temperature.

#### 4 Conclusions

The effect of hydrogen peroxide on methane/air premixed flames are numerically investigated under the atmosphere condition. Hydrogen peroxide is used as fuel additive or oxidizer for three different conditions: (1) replacing partial air by  $H_2O_2$ , (2) adding  $H_2O_2$  as fuel additive, (3) using  $H_2O_2$  as an oxidizer but with different concentrations. Results show that the laminar burning velocities are obviously increased no matter  $H_2O_2$  is used as fuel additive or oxidizer. The adibatic temperatures are also increased with the addition of  $H_2O_2$ . However, when  $H_2O_2$  is used as fuel additive, the adiabatic flame temperature is not increased obviously, especial in the fuel-lean conditions.

The effects of  $H_2O_2$  on the OH, CO, NO and NO<sub>2</sub> are also investigated. OH concentration is always increased unless lower  $H_2O_2$  concentration is used as an oxdizer (30% in the study). The increase of OH concentration enhances the reaction rate and then affects the laminar burning velocity. For CO emission, the CO emission is decreased with adding  $H_2O_2$  as fuel additive. However, using  $H_2O_2$  to replace air will increase CO emission. It is due to the coversion of CO<sub>2</sub> to CO in the high temperature condition. If  $H_2O_2$  is used as an oxidizer with lower concentrations (30% and 40%), CO emission is decreased. As to NO<sub>x</sub> emission, using  $H_2O_2$  as an oxidizer will never produce NO<sub>x</sub>. For the other two cases, the NO<sub>x</sub> emission is always increased due to the increased flame temperature.

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## References

- [1] Mcmanus, K.R., T. Poinsot, T., and Candel, S.M., (1993) "A review of active control of combustion instabilities" Prog. Energy Combust. Sci., 19: 1.
- [2] Proscia, B. and Peraccio, Z., (1998) "NOx As a Function of Fuel for C1-toC16 Hydrocarbons and Methanol Burned in a High Intensity, Lean-Premixed, Combustion Reactor", ASME Paper # 98-GT-269.
- [3] Feikema, D., Chen, R. H., Driscoll, J. F., (1989) "Enhancement of flame blowout limits by the use of swirl." AIAA 89-0158.
- [4] Pfefferle, W. C., Pfefferle, L. D., (1986) "Catalytically stabilizaed combustion." Prog. Energy Combust. Sci., 12: 25.
- [5] Zabetakis, M. G., "Flammability characteristics of combustible gases and vapors." U.S. Department of Mines Bulletin 627.
- [6] Golovitchev, VI, Pilia ML, Bruno, C., (1996) "Autoignition of methane mixtures: the effect of hydrogen peroxide.", Journal of Propulsion and Power 12(4):699.
- [7] Ting, D. K., Reader, G. T., (2005) "Hydtogen peroxide for improving permixed methaneair combustion." Energy, 30:313.
- [8] Kim, I., Park, J., Goto, S., (2000) "Conversion of nitric oxide to nitrogen dioxide using hydrogen peroxide" SAE Paper 2000-01-1931.
- [9] Born C, Peters N., (1998) "Reduction of soot emission at a DI diesel engine by additional injection of hydrogen peroxide during combustion." SAE Paper 982676.
- [10] Martinez AI, Corredor LF, Tamara W. (1997) "Reduction of combustion emissions using hydrogen peroxide in a pilot scale combustion chamber." Proceedings of the 1997 Air and Waste Management Association's 90th Annual Meeting and Exhibition, Paper 97-TP30B.01.
- [11] Smith G, Golden D, Frenklach M, Moriaty N, Eiteneer B, Goldenber M, Bowman C, Hanson R, Song S, Gardiner W, Lissianski V, Qin Z, GRI-Mech 3.0, 1999, <u>http://euler.me.berkeley.edu/gri\_mech</u>.



Fig. 1 Profiles of temperature and species concentration of stoichiometric  $CH_4/air/H_2O_2$  flames. (a)  $CH_4$  and 100% air, (b) $CH_4$ , 85% air and 15%  $H_2O_2$ .



3000 Laminar burning velocity 2800 2 Laminar burning velocity (m/s) perature 2600 ten e flar oatic 2200 P 2000 0 L 20 100 60 80 H2O2 concentration

Fig. 3 The laminar flame speed and adiabatic flame temperature of stoichiometric methane/  $H_2O_2$  flames with different  $H_2O_2$  concentration.



Fig. 2 The laminar flame speed and adiabatic flame temperature of methane/air flames with different percentages of air replaced by  $H_2O_2$ .

Fig. 4 The laminar flame speed and adiabatic flame temperature of methane/air/ $H_2O_2$  flames with different percentages of  $H_2O_2$  additions.



Pure air replacing 10% air replacing 20% air

eplaci

ng 30% air

0.07

0.06

0.05

0.02

0.01 0

0.06

0.05

(b)

CO mole fraction 0.04 0.03 (a)



Pure air add 10%H2O2 add 20%H2O2 add 30%H2O2 add 40%H2O2 add 50%H2O2 0.04 mole fraction 0.03 8 0.02 0.01 0 Axial distance (cm) 8 0.1 Pure air Pure air 30% H2O2 40% H2O2 60% H2O2 80% H2O2 100% H2O2 (c) 0.08 0.04 Contraction 8 0.02 4 6 8 10 0 L Axial distance (cm) Fig. 6 The effect of H<sub>2</sub>O<sub>2</sub> on CO mole fraction

Áxial distance (cm)

Fig. 5. The effect of H<sub>2</sub>O<sub>2</sub> on OH mole fraction for three cases: (a) replacing partial air by  $H_2O_2$ (b) adding extra  $H_2O_2$  (c)  $H_2O_2$  as an oxidizer with different concentrations.



Fig. 7 The effect of  $H_2O_2$  on NO mole fraction for two cases: (a) replacing partial air by  $H_2O_2$ (b) adding extra  $H_2O_2$ .



for three cases: (a) replacing partial air by  $H_2O_2$ 

(b) adding extra  $H_2O_2$  (c)  $H_2O_2$  as oxidizer with

different concentrations.

Fig. 8. The effect of  $H_2O_2$  on  $NO_2$  mole fraction for two cases: (a) replacing partial air by  $H_2O_2$ (b) adding extra  $H_2O_2$ .